

POWDER METAL COMPOSITION AND METHOD FOR PRODUCING
COMPONENTS THEREOF

Field of the invention

The present invention concerns powder metallurgy. More specifically the present invention concerns a cobalt-based powder metal composition and a method for
5 producing components thereof, especially for heavy duty applications.

Background of the invention

Cobalt-based alloys, such as Stellite® (Trade Mark
10 for Co-Cr-W alloys) are hard alloys that are extremely resistant to many forms of wear. Products of these alloys show high hardness over a wide temperature range and are resistant towards corrosion. These products are used for inter alia casting of various kinds of components such as
15 machine parts (bearing shells, valve seat inserts etc) or other components where high density, high strength and wear resistance are required.

Cast material often suffers from micro structural defects and carbide segregation. Carbide segregation
20 leads to inhomogenously distributed hard phases. Disadvantages with such materials are lack of fracture toughness and poor machinability.

Powder metallurgy (PM) products generally possess a more homogenous microstructure than cast products.
25 Further advantages with the PM production method are that costly machining into final shape may be excluded or minimized in comparison with traditional casting methods and that the method is more suitable for producing large quantities of small articles.

30 Attempts have been made over the years to produce cobalt-based products using the PM technology. Thus the US patent 4129444 discloses a process wherein atomised Co-based alloy powders are coated with a binder and then consolidated to produce discrete bodies that are dried,

crushed and screened to obtain agglomerates. The agglomerates are pressed into green compacts which are sintered at high temperature. Furthermore the US patent 5,462,572 discloses a powder metallurgy component prepared of a gas atomised Co-Cr-Mo alloy powder. The alloy powder is filled in a canister and baked in vacuum to degas the powder and the powder filled canister is thereafter consolidated, preferably by hot isostatic pressing (HIP).

10

Objects of the invention

An object of the invention is to provide a new Co-based powder metal composition which can be used in conventional PM processes.

15

Another object is to provide a Co-based powder metal composition with high compactibility which can be compacted to high green density and high green strength.

Still another object is to provide a green body of a cobalt based alloy which can be machined before sintering.

20

A further object is to provide a powder metal composition which can be compacted and sintered to high density without high sintering temperatures.

25

Summary of the invention

These object as well as other objects that will be apparent from the description below, have now been obtained according to the present invention by providing a new Co-based powder metal composition. Critical

30

features of this composition are that the composition comprises a Co-based pre-alloyed powder with irregularly shaped particles admixed with graphite. Furthermore the Co-based pre-alloyed powder should include less than 0.3% by weight of carbon and at least 15% by weight Cr.

35

The Co-based pre-alloyed powder preferably comprises at least 30% by weight and preferably less than 80% by weight Co.

The invention also concerns a method comprising the steps of providing a powder metal composition according to the invention and compacting the composition in a die at a pressure of at least 400 MPa to a component of
5 desired shape.

Detailed description of the invention

The Co-based pre-alloyed powder in the composition according to the invention may be produced by subjecting
10 a melt having the desired composition to atomising by water.

The Co-based pre-alloyed powder according to the invention comprises less than 0.3% by weight carbon. The carbon content of the powder is however preferably less
15 than 0.1% by weight, and most preferably less than 0.05% by weight (i.e. essentially free from C except for inevitable impurities).

The Co-based pre-alloyed powder comprises at least 15% by weight and preferably less than 35% by weight Cr.
20 The addition of Cr improves the strength of the Cobalt matrix by solution hardening and/or carbide formation. These effects are further improved by the addition of W and/or Mo.

Other elements which may be included in the Co-based
25 pre-alloyed powder may be chosen from Ni, Fe, Si, Mn, V and B.

A preferred pre-alloyed powder according to the invention comprise: 5-35% by weight Cr, 0-20% by weight W, 0-25% by weight Ni, 0-5% by weight Si, 0-5% by weight
30 Fe, 0-10% by weight Mo, balance Co and less than 0.3% by weight C.

Another preferred powder according to the invention further comprise 0-3% by weight Mn, 0-4% by weight V and 0-4% by weight B.

35 A powder metal composition according to the invention comprises a pre-alloyed powder according to the invention admixed with graphite. The amount of graphite

addition depends on the desired content of carbides and on the content of carbide forming elements. The graphite content is preferably at least 0.5% by weight, more preferably at least 0.7% by weight and preferably less than 3% by weight.

The powder metal composition may further comprise one or more additives selected from the group consisting of alloying elements, lubricants, processing aids and binders.

Other elements may be added for improving properties or reducing costs.

The used lubricant plays an important role for the achieved green properties. Good results have been achieved with Kenolube™ (available from Höganäs AB, Sweden), amide wax, metal stearates and other commonly used lubricants.

The processing aids used in the powder metal composition according to the invention may consist of talc, forsterite, manganese sulphide, sulphur, molybdenum disulphide, boron nitride, tellurium, selenium, barium difluoride and calcium difluoride, which are used either separately or in combination.

The powder metal composition according to the invention is filled in a die and compacted at a pressure of at least 400 MPa to a component of desired shape. This compaction yields a component with high green strength and green density and the component may even be green machined at this stage. This is an advantage as the material in the final sintered component are hard and difficult to machine.

The component is sintered at a temperature of at least 1080°C, preferably in protective atmosphere or vacuum.

The components produced of the powder according to the invention and according to the method of the invention are especially suited for heavy-duty applications, such as valve seat inserts for engines

where the valve seats need to last the life time of the engine, without replacement or service.

The following example, which is not intended to be limiting, present certain embodiments of the present invention.

Example

The test mixtures (mix 1-5) listed in table 2 and 3 were prepared from the water atomised pre-alloyed powders in table 1 (% by weight).

Table 1

| | Co | Cr | Ni | W | Si | Fe | C |
|-----|------|------|------|------|------|------|------|
| 285 | 36.4 | 25.8 | 23.0 | 12.5 | 1.12 | 1.19 | 0.01 |
| 286 | 34.5 | 26.1 | 23.0 | 12.5 | 1.16 | 1.16 | 1.60 |

15

The pre-alloyed powders were further admixed with lubricants, alloying elements and processing aids according to table 2 and 3. In test mix 1, 3 and 4, 1.7% by weight graphite was further included. TRS-samples, according to ISO 3995, were moulded. The compacting operation was performed with the three different types of samples at 600 and 800 MPa respectively.

The resulting components were tested for green density (GD) and green strength (GS). After sintering at 1120°C for 30 minutes in a 90% N₂/10% H₂ atmosphere the components were tested for sintered density (SD) and hardness (Hv10). Table 4 and 5 discloses the results of the tests.

Table 2

| Mix | 1 (% by weight) | 2 (% by weight) |
|---------------------|-----------------------|-----------------------|
| Powder | Balance Powder 285 | Balance Powder 286 |
| Lubricant | 40 PEO:60 ORG* 0.8 | 40 PEO:60 ORG* 0.8 |
| Graphite (KS 44) | 1.7 | 0 |

5 *40% Polyethyleneoxide:60% Orgasol

TABLE 3

| Mix | 3 (% by weight) | 4 (% by weight) | 5 (% by weight) |
|---------------------|-----------------------|-----------------------|-----------------------|
| powder | Balance Powder 285 | Balance Powder 285 | Balance Powder 286 |
| Fe (MH 80,23) | 10 | 10 | 10 |
| Cu (325) | 5 | 5 | 5 |
| MoS ₂ | 1 | 1 | 1 |
| Lubricant | 40 PEO:60 ORG* 0.8 | Kenolube™ 0.8 | 40 PEO:60 ORG* 0.8 |
| Graphite (KS 44) | 1.7 | 1.7 | 0 |

10 *40% Polyethyleneoxide:60% Orgasol

TABLE 4

| Mix | 1 | | 2 | |
|---------------------------|------|------|------|-----|
| Compaction Pressure (MPa) | 600 | 800 | 600 | 800 |
| GD (g/cm ³) | 6.70 | 7.00 | 5.73 | BF* |
| GS (MPa) | 13.1 | 19.7 | 1.3 | BF* |

*Bars Fractured on ejection

5

TABLE 5

| Mix | 3 | | 4 | | 5 | |
|---------------------------|-------|-------|------|------|------|------|
| Compaction Pressure (MPa) | 600 | 800 | 600 | 800 | 600 | 800 |
| GD (g/cm ³) | 6.76 | 7.04 | 6.88 | 7.13 | 6.07 | 6.39 |
| GS (MPa) | 15.57 | 21.09 | 10.2 | 13.5 | 2.64 | 4.39 |
| SD (g/cm ³) | 6.62 | 6.91 | nm | nm | 6.11 | 6.40 |
| Hv10 | 137 | 175 | nm | nm | 103 | 129 |

nm=not measured

10

Compaction of mix 2 and to some extent mix 5 did not work, the components exhibited bad surfaces and frequent edge cracks and were too fragile to handle.

Compaction of mix 1, 3 and 4, without C in the pre-alloyed powder, showed a great improvement of the compressibility, as can be seen in table 4 and 5, and high green strengths and green densities were achieved for the resulting components. Components with thin walls normally require a green strength of at least 7 MPa to enable handling. Green strengths above 20 MPa normally enable green machining.

The sintered mix 3 components exhibit a higher density and hardness (Hv10) than mix 5 components.

Metallographic studies of the sintered components showed that components made from mix 3 and 5 have similar

25

structures. It is thus possible to create the desired carbide structures in mix 3 components during sintering.

A comparison between mix 3 and mix 4 in table 5 demonstrates the influence of lubricants on the green strength and green density of the compacted components. 5 Kenolube™ gives a higher density than the mix of Polyethyleneoxide and Orgasol which enables better performance in the sintered state.